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TRANSPORTS IN THE
PACIFIC EQUATORIAL COUNTERCURRENT

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By

Thomas Robert Kendall

Thesis Committee:

Klaus Wyrtki, Chairman
Vernon E. Brock
Brian F. Pasby
Charles W. Thomas
George P. Woollard

b77495

Hawh.
Q111
H3
no. 542
Cop. 2

We certify that we have read this thesis and that in our opinion it is satisfactory in scope and quality as a thesis for the degree of Master of Science in Oceanography.

THESIS COMMITTEE

Klaus Ylki

Chairman

Geo. T. Woodland

V. E. Broder

Russ Dyer

Charles W. Thomas

ABSTRACT

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Volume transports in the Pacific Equatorial Counter-current have been estimated by geostrophic methods. A thermoclinic method using only bathythermograph sections to estimate transports is introduced and evaluated. Compilation of transports in the countercurrent along 79 hydrographic sections and estimated transports along 50 bathythermograph sections are presented. It is shown that the average transport of the countercurrent decreases almost linearly from approximately 40 million cubic meters per second in the western portion of the Pacific Ocean to termination at the coast of Central America. No conclusive variations of seasonal transports were found.

TABLE OF CONTENTS

	Page
ABSTRACT	iii
LIST OF TABLES	v
LIST OF ILLUSTRATIONS	vi
INTRODUCTION	1
THERMOCLINIC TRANSPORT	3
GEOSTROPHIC TRANSPORT	6
RELATIONSHIP BETWEEN THERMAL STRUCTURE AND FLOW . . .	8
COMPARISON BETWEEN GEOSTROPHIC AND THERMOCLINIC TRANSPORTS	9
RESULTS	11
ACKNOWLEDGEMENTS	13
BIBLIOGRAPHY	14

LIST OF TABLES

TABLE		Page
I.	TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTERCURRENT	18
II.	THERMOCLINIC TRANSPORT OF THE PACIFIC EQUATORIAL COUNTERCURRENT	26
III.	TABULATED TRANSPORTS BY MONTH AND LONGITUDE . . .	29

LIST OF ILLUSTRATIONS

FIGURE	Page
1.	MERIDIONAL SECTION OF THE PACIFIC EQUATORIAL COUNTERCURRENT. 30
2.	VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A <u>VITYAZ</u> SECTION AT 142° E (IDENTIFICATION NO. 44) 31
3.	VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A <u>STRANGER</u> SECTION AT 175°W (IDENTIFICATION NO. 12) 32
4.	VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A <u>HUGH M. SMITH</u> SECTION AT 150°W (IDENTIFICATION NO. 8) 33
5.	VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A <u>S. F. BAIRD</u> SECTION AT 115°W (IDENTIFICATION NO. 49). 34
6.	GEOSTROPHIC TRANSPORT VERSUS TRANSPORT FUNCTION WITH LONGITUDE REGIONS AND A FACTOR $k = 1.5$ NOTED 35
7.	FACTOR K VERSUS LONGITUDE. 36
8.	POSITIONS OF COUNTERCURRENT SECTIONS INDICATING RANGE AND TRANSPORT MAGNITUDES ($10^6 M^3/SEC.$) FOR THE MONTHS OF JANUARY THROUGH JUNE. CIRCLED IDENTIFICATION NUMBERS REFER TO TABLES I AND II 37

LIST OF ILLUSTRATIONS (Continued)

FIGURE		Page
9.	POSITIONS OF COUNTERCURRENT SECTIONS INDICATING RANGE AND TRANSPORT MAGNITUDES ($10^6\text{M}^3/\text{SEC.}$) FOR THE MONTHS OF JULY THROUGH DECEMBER. CIRCLED IDENTIFICATION NUMBERS REFER TO TABLES I AND II	38
10.	GEOSTROPHIC AND THERMOCLINIC TRANSPORTS VERSUS LONGITUDE WITH LIMITED SECTIONS NOTED . . .	39
11.	MEAN TRANSPORTS FOR INCREMENTS OF LONGITUDE. . .	40
12.	SEASONAL TRANSPORTS VERSUS LONGITUDE	41

INTRODUCTION

The Pacific Equatorial Countercurrent flows from west to east across the entire Pacific Ocean, a few degrees north of the equator. It is relatively narrow, 300 to 700 kilometers wide, and it separates the broader, westward-flowing North and South Equatorial Currents. As such, it acts as a boundary between the great anticyclonic gyres of the North and South Pacific. Surface components of the countercurrent have been recognized and presented on charts for over a century. However, analysis of the volume transports has only recently been initiated.

Geostrophic transports have been estimated by Sverdrup et al (1942), Jerlov (1956), Austin et al (1956), and Tsuchiya (1961). Knauss (1961) demonstrated that velocity measurements in the countercurrent agree with geostrophic calculations to a first approximation. These results suggest that geostrophic transports, a function of the slope of geopotential surfaces, are a measure of actual transports. Montgomery and Stroup (1962), in a more comprehensive analysis, discuss volume transports as derived from geostrophic calculations. In addition to summarizing previous studies, they demonstrate agreement with measured current values.

Extensive efforts have been made in recent years to collect oceanographic data in the Pacific equatorial regions, resulting in a large accumulation of bathythermo-

graph and, to a lesser extent, hydrographic data. A method will be introduced by which transports in the countercurrent can be estimated solely from bathythermograph data. A comparison between geostrophically calculated transports and values derived from the thermal structure will demonstrate the validity of this new method.

THERMOCLINIC TRANSPORT

A meridional section of the countercurrent is characterized by a sea surface sloping away from the equator and an underlying thermocline which slopes toward the equator. (See Figure 1.) The thermal gradient is greatest between 25° and 15° centigrade, with the 20° centigrade isotherm indicating the mean, as shown in Figures 2 through 5. This thermocline separates two distinct water densities, a well-mixed upper layer and a stable lower layer. If it can be shown that a relationship exists between the slope of the thermocline and geostrophic transport, it may be possible to infer an estimate of actual transport, as suggested by Wyrtki (1964).

If the ocean consists of two density layers separated by a thermocline with the lower layer at no motion, then the eastward velocity component u in the upper layer according to Sverdrup et al (1942) is given by

$$(1) \quad fu = gi_y \frac{\Delta\rho}{\rho} = g \frac{\Delta\rho}{\rho} \frac{\Delta Z}{\Delta y}$$

where $f = 2\omega \sin\phi$ is the Coriolis parameter, g is the acceleration of gravity, ρ the density, $\Delta\rho$ the density difference between the upper and the lower layer, and $i_y = \frac{\Delta Z}{\Delta y}$ is the slope of the boundary between the two layers in the meridional direction. The volume transport T_{bt} to the east in the upper layer is given by

$$(2) \quad T_{bt} = \bar{u} \bar{Z} \Delta y$$

where \bar{Z} is the average depth of the upper layer and Δy is the meridional width of the countercurrent. From equations 1 and 2 follows

$$(3) \quad T_{bt} = \frac{g \Delta \rho}{2 \omega \sin \phi} \cdot \frac{\Delta \rho}{\rho} \cdot \bar{Z} \Delta Z$$

For the meridional section described in Figure 1, this is

$$(4) \quad T_{bt} = \frac{g \Delta \rho}{4 \omega \rho} \frac{(Z_S - Z_N)(Z_S + Z_N)}{\sin \phi}$$

where Z_S and Z_N are the depths of the upper layer at the south and north boundaries of the countercurrent. Consequently, a relationship between the transports in the upper layer (T_{bt}) and values of Z_S and Z_N should exist, having the form

$$(5) \quad T_{bt} = k \frac{(Z_S - Z_N)(Z_S + Z_N)}{\sin \phi}$$

where

$$k = \frac{g \Delta \rho}{4 \omega \rho}$$

For the countercurrent, the magnitude of k can be estimated. Assuming a density $\rho_1 = 1.023$ for the upper layer and $\rho_2 = 1.027$ for the lower layer, $g = 9.81$ meters per second squared, and $\omega = 0.729 \times 10^{-4}$ per second, gives $k = 1.5 \times 10^2$ meters per second. By comparison between geostrophic transports and values of Z_S and Z_N , it should be shown that such a factor k exists and is applicable at

least to certain portions of the countercurrent.

GEOSTROPHIC TRANSPORT

A total of 79 hydrographic sections were used to calculate geostrophic transport in the countercurrent. An arbitrary level of no motion was chosen at 500 meter depth. Montgomery and Stroup (1962) sustained a level at 300 meters and suggested that deepening the base would lower the calculated transport. Austin et al (1956) selected 400 meters, having previously shown that a deeper reference level at 500 meters did not significantly change the velocity profile in the region of the countercurrent. Jerlov (1956) states that appreciable current velocities are found as deep as 400 meters, the layer of no motion falling between 500 and 900 meters. Sverdrup (1944) used 700 meters with the note that accidental errors of observation exercise a greater influence at depths below this level.

The equation utilized in this study to compute geostrophic transport T_g is

$$(6) \quad T_g = 10 \sum_y \frac{1}{f} \sum_Z (\Delta \bar{D}_A - \Delta \bar{D}_B) \Delta Z$$

where ΔD is the anomaly of dynamic height at the individual hydrographic station and ΔZ is the interval between standard depths. The summation is done vertically between adjoining hydrographic stations, an average Coriolis parameter for the respective stations has been used, and then individual columns have been added to obtain the total transport of the countercurrent. Entire columns of

negative transport have not been included in the summation. In the lower portions of the countercurrent near the northern and southern boundaries, occasionally geostrophic flow to the west is observed. This flow has been included in the transport computations, but sections where its effect is greater than 10% are marked in Table I by the symbol +. The results of the geostrophic computations are given in Table I.

In some instances, the hydrographic sections are limited, and may not completely cross the countercurrent. The implications are that transport estimates may be low. These limited sections are noted in Figures 8 and 9. Arcs of a circle at the end of a section indicate the limit of data sampling.

Data sources not referenced in the text are included in the bibliography.

RELATIONSHIP BETWEEN THERMAL STRUCTURE AND FLOW

In order to demonstrate that geostrophic currents and transport are in fact associated with the upper layer in the thermal structure of a meridional section of the countercurrent, Figures 2 through 5 have been prepared. The vertical distribution of temperature at the northern and at the southern boundary of the countercurrent shows the division into an upper layer of high temperature and a lower layer with temperatures less than 10° centigrade. The 20° centigrade isotherm represents approximately the center of the thermocline and, therefore, is a measure of the thickness of the upper layer. It is evident from the four figures that the depth of the upper layer decreases across the Pacific Ocean from west to east, being more than 150 meters thick at 142° east longitude (Figure 2) and less than 100 meters at 115° west longitude (Figure 5). On the right-hand side of each of the four figures, the differences of dynamic heights across the countercurrent are plotted as a function of depth. Their distribution demonstrates that the strong flow in the countercurrent is concentrated in a relatively shallow layer near the sea surface and that this layer corresponds to the warm layer in the thermal structure. On the basis of these comparisons, it can be justified to compare geostrophic transports with the thickness of the upper layer and the slope of the thermocline.

COMPARISON BETWEEN GEOSTROPHIC AND THERMOCLINIC TRANSPORTS

Geostrophic transports calculated according to equation 6 will be compared with thermoclinic transports according to equation 5. Define a transport function as

$$(7) \quad \left[\frac{T_{bt}}{k} \right] = \frac{(Z_S - Z_N)(Z_S + Z_N)}{\sin \bar{\phi}}$$

Evaluation of this transport function requires the knowledge of the depths of the 20° centigrade isotherm Z_S and Z_N at the south and north boundaries of the countercurrent and its mean latitude $\bar{\phi}$. Dividing geostrophic transport by the transport function gives an estimate of the factor k .

$$\frac{T}{\left[\frac{T_{bt}}{k} \right]} = k$$

Data for calculation of the transport functions are taken from the same hydrographic sections for which geostrophic transports have been computed. The depths of the 20° centigrade isotherm are obtained by linear interpolation. In a few cases, the bounds of the slope of the thermocline did not coincide with the bounds of the dynamic heights of the sea surface. In order that the method be consistent with subsequent evaluation of independent bathythermograph sections, the geostrophic transport is calculated within the bounds of a sloping sea surface, and the mean latitude for the transport function is taken midway between the bounds of the lowest and highest ends of the

sloping thermocline. The values of the transport function are also listed in Table I.

A plot of geostrophic transport versus the transport function is presented in Figure 6 and shows a more or less linear relationship. The straight line with a factor of $k = 1.5 \times 10^2$ meters per second corresponds with the previously estimated value of k . Factor k versus longitude is given in Figure 7. Three distinct regions are noted. From 180° east to 120° west longitude, the values cluster about $k = 1.5$. To the west of 180° , the values are more dispersed though $k = 1.5$ may be inferred. Between 110° west and 85° west, values of k are much larger. It is in this eastern oceanic region that the countercurrent finally disperses, as shown in the maps of surface currents by Wyrтки (1965).

This study indicates that volume transports in the countercurrent may be estimated from meridional sections of bathythermograph data. The only information required are the depths of the lowest and the highest points in the thermocline (20° centigrade isotherm) and the mean latitude.

RESULTS

The equation for thermoclinic transport has been applied to 50 bathythermograph sections and the estimated thermoclinic transports are listed in Table II. A factor $k = 1.5 \times 10^2$ meters per second was used throughout. A summary by month and against latitude and longitude of counter-current sections used in this study is presented in Figures 8 and 9. Positions and ranges are mapped. Calculated transports in millions of cubic meters per second are indicated. Circled identification numbers refer to Tables I or II. South and/or north end points of limited sections are indicated by arcs of a circle.

Transports as a function of longitude are presented in Figure 10. The method of calculation and limited sections are noted. The distribution of transports suggests an upper bound which seems to be a more or less linear function with longitude. Figure 7 shows k factors around 6×10^2 meters per second for the interval 110° west to 85° west. If such a factor is applied to the bathythermograph sections in this interval, the estimated transports notably exceed that upper bound. Mean transports for increments of longitude are illustrated in Figure 11. An average flow of 40 million cubic meters per second west of 180° decreases to 20 million cubic meters per second by 140° west longitude. Volume transports clearly decrease as the countercurrent flows eastward. Sverdrup et al (1942) had suggested to the

contrary.

Some seasonal variations in the transports with longitude are presented in Figure 12 and Table III. In the western equatorial Pacific Ocean, the flow appears to be a regular feature. In mid-ocean, transports seem to be strong during September through February and weak March through August. At its eastern extremity during March through May (Figure 12) decrease of values indicate that the countercurrent would terminate before reaching 100° west longitude. Flow east of 100° west is in evidence during other seasons.

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TABLE I.

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section</u> (P. E. C. C.)		<u>Geostrophic Transport</u> ($10^6\text{m}^3/\text{sec.}$)	<u>Transport Function</u> ($10^4\text{m}^2/\text{sec.}$)	<u>Factor K</u> (10^2)	<u>I. D. No.</u>
ALBATROSS (Oct.1947)	4°49'N 130°52'W	9°50'N 128°13'W	39.83	29.1	1.37	18
ALBATROSS (Nov.1947)	5°47'N 149°42'W	8°43'N 148°36'W	23.36	17.0	1.37	19
ALBATROSS (Dec.1947)	2°54'N 173°17'W	8°40'N 169°28'W	61.60+	34.2	1.80	20
S.F. BAIRD Eastropic (Oct.1955)	7°02'N 115°40'W	12°05'N 116°09'W	12.50	7.2	1.74	48
S.F. BAIRD Eastropic (Oct.1955)	6°22'N 115°24'W	10°58'N 115°58'W	10.74+	7.4	1.45	49
S.F. BAIRD Eastropic (Nov.1955)	7°33'N 87°21'W	8°24'N 87°35'W	3.44	0.6	5.73	50
S.F. BAIRD Eastropic (Nov.1955)	7°51'N 84°34'W	9°13'N 84°51'W	1.43+	0.6	2.38	51
S.F. BAIRD Eastropic (Nov.1955)	6°54'N 84°21'W	8°54'N 84°42'W	1.19+	1.8	.66	52
S.F. BAIRD Eastropic (Dec.1955)	3°49'N 90°37'W	8°54'N 89°36'W	13.42	1.9	7.10	53
S.F. BAIRD CRD (Nov.1959)	6°45'N 86°44'W	8°17'N 88°16'W	5.73+	1.0	5.73	71
S.F. BAIRD Tethys (June 1960)	4°34'N 130°58'W	7°47'N 129°37'W	15.90	9.9	1.60	72
S.F. BAIRD Tethys (July 1960)	4°57'N 142°55'W	9°45'N 146°48'W	20.60	11.5	1.79	73
CARNEGIE 7 (May 1929)	4°22'N 176°33'W	8°05'N 178°48'W	3.73+	9.3	.40	76

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P. E. C. C.)</u>	<u>Geostrophic Transport ($10^6 \text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4 \text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I. D. No.</u>
CARNEGIE 7 (Oct.1929)	$3^{\circ}01'N$ — $10^{\circ}05'N$ $149^{\circ}46'W$ — $139^{\circ}44'W$	42.43	27.4	1.55	75
DAIFUJI-MARU (July 1956)	$3^{\circ}00'N$ — $7^{\circ}30'N$ $175^{\circ}11'E$ — $162^{\circ}36'E$	43.50	29.7	1.46	16
DAIFUJI-MARU (Aug.1956)	$4^{\circ}14'N$ — $10^{\circ}00'N$ $142^{\circ}41'W$ — $141^{\circ}24'W$	23.80	15.8	1.51	16A
HOKUSEI-MARU 3 (Jan.1958)	$1^{\circ}52' - 6^{\circ}28'N$ $135^{\circ}00'E$	22.50	25.9	.87	27
HOKUSEI-MARU 3 (Jan.1958)	$2^{\circ}50'N$ — $7^{\circ}36'N$ $136^{\circ}26'E$ — $135^{\circ}57'E$	10.59	17.7	.60	28
HORIZON Eastropic (Oct.1955)	$6^{\circ}01'N$ — $11^{\circ}00'N$ $120^{\circ}46'W$ — $120^{\circ}56'W$	11.84	6.6	1.79	54
HORIZON Eastropic (Oct.1955)	$8^{\circ}00' - 9^{\circ}58'N$ $111^{\circ}30'W$	6.73	2.8	2.40	55
HORIZON Eastropic (Oct.1955)	$5^{\circ}40' - 10^{\circ}00'N$ $111^{\circ}00'W$	7.46	5.6	1.33	56
HORIZON Eastropic (Nov.1955)	$7^{\circ}54'N$ — $9^{\circ}29'N$ $89^{\circ}15'W$ — $88^{\circ}25'W$	1.34	0.3	5.36	57
HORIZON Eastropic (Nov.1955)	$6^{\circ}55'N$ — $9^{\circ}00'N$ $83^{\circ}38'W$ — $84^{\circ}32'W$	4.89	2.0	2.45	58
HORIZON Eastropic (Nov. 1955)	$4^{\circ}05'N$ — $6^{\circ}52'N$ $77^{\circ}45'W$ — $78^{\circ}54'W$	4.71	2.8	1.68	59
HORIZON Eastropic (Dec.1955)	$4^{\circ}08'N$ — $9^{\circ}03'N$ $102^{\circ}02'W$ — $104^{\circ}34'W$	19.92	3.0	6.64	60
HORIZON Equapac (Aug.1956)	$2^{\circ}59' - 6^{\circ}30'N$ $157^{\circ}00'E$	47.26	26.2	1.80	10

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P. E. C. C.)</u>	<u>Geostrophic Transport ($10^6 \text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4 \text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I. D. No.</u>
HORIZON Equapac (Aug.1956)	$1^{\circ}56' - 8^{\circ}01' \text{N}$ $164^{\circ}00' \text{E}$	45.65+	18.6	2.45	11
HORIZON Downwind (Oct.1957)	$3^{\circ}14' \text{N} - 7^{\circ}08' \text{N}$ $130^{\circ}03' \text{W} - 129^{\circ}16' \text{W}$	26.52	12.4	1.66	63
HORIZON Downwind (Feb.1958)	$2^{\circ}00' \text{N} - 10^{\circ}02' \text{N}$ $115^{\circ}32' \text{W} - 118^{\circ}58' \text{W}$	18.23	7.9	2.31	64
HORIZON Dorado (July 1959)	$7^{\circ}32' - 9^{\circ}47' \text{N}$ $120^{\circ}00' \text{W}$	7.85+	5.3	1.48	69
HORIZON Dorado (July 1959)	$6^{\circ}00' - 10^{\circ}00' \text{N}$ $120^{\circ}00' \text{W}$	6.30+	6.0	1.05	70
HORIZON Step I (Dec.1960)	$1^{\circ}59' - 10^{\circ}05' \text{N}$ $95^{\circ}00' \text{W}$	15.42+	3.1	4.97	74
KAGOSHIMA-MARU Equapac (Aug.1956)	$3^{\circ}02' - 8^{\circ}00' \text{N}$ $130^{\circ}00' \text{E}$	68.45	28.1	2.44	14
KAGOSHIMA-MARU (April 1958)	$4^{\circ}00' - 7^{\circ}00' \text{N}$ $151^{\circ}00' \text{E}$	25.65	10.3	2.49	33
KAGOSHIMA-MARU (April 1958)	$2^{\circ}00' \text{N} - 9^{\circ}59' \text{N}$ $153^{\circ}00' \text{E} - 151^{\circ}00' \text{E}$	68.83	21.2	3.25	34
KEITEN-MARU Equapac (July 1956)	$1^{\circ}49' - 6^{\circ}00' \text{N}$ $135^{\circ}00' \text{E}$	86.38	47.5	1.82	15
SATSUMA Equapac (Aug.1956)	$2^{\circ}03' - 6^{\circ}27' \text{N}$ $151^{\circ}00' \text{E}$	37.45	27.6	1.36	23
SATSUMA Equapac (Aug.1956)	$2^{\circ}13' \text{N} - 6^{\circ}32' \text{N}$ $150^{\circ}00' \text{E} - 147^{\circ}49' \text{E}$	20.68+	19.1	1.08	24
SATSUMA Equapac (Aug.1956)	$2^{\circ}04' \text{N} - 5^{\circ}03' \text{N}$ $141^{\circ}05' \text{E} - 142^{\circ}19' \text{E}$	58.58	44.0	1.33	25

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P.E.C.C.)</u>	<u>Geostrophic Transport ($10^6\text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4\text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I. D. No.</u>
SATSUMA Equapac (Aug.1956)	$2^{\circ}03' - 6^{\circ}30'N$ $140^{\circ}00'E$	39.85	29.1	1.37	26
SATSUMA (Feb.1958)	$4^{\circ}00' - 7^{\circ}00'N$ $147^{\circ}00'E$	15.80+	15.2	1.04	32
H.M. SMITH 2 (Feb.1950)	$6^{\circ}07' - 11^{\circ}03'N$ $172^{\circ}00'W$	24.78	15.6	1.59	1
H.M. SMITH 2 (Feb.1950)	$6^{\circ}00' - 9^{\circ}55'N$ $158^{\circ}00'W$	20.20	12.9	1.57	2
H.M. SMITH 5 (Aug.1950)	$5^{\circ}00'N - 9^{\circ}00'N$ $158^{\circ}00'W - 157^{\circ}55'W$	22.06	18.8	1.17	3
H.M. SMITH 5 (July 1950)	$3^{\circ}00' - 8^{\circ}00'N$ $172^{\circ}00'W$	25.77	18.0	1.43	5
H.M. SMITH 8 (Jan.1951)	$3^{\circ}02' - 9^{\circ}00'N$ $158^{\circ}00'W$	28.69	18.9	1.52	4
H.M. SMITH 8 (Feb.1951)	$4^{\circ}58'N - 6^{\circ}44'N$ $165^{\circ}35'W - 165^{\circ}23'W$	16.71	10.7	1.56	6
H.M. SMITH 8 (Mar.1951)	$4^{\circ}56' - 10^{\circ}02'N$ $172^{\circ}00'W$	19.65	15.9	1.24	7
H.M. SMITH 11 (Sept.1951)	$5^{\circ}00' - 10^{\circ}00'N$ $150^{\circ}00'W$	26.4	20.2	1.31	8
H.M. SMITH 14 (Jan.1952)	$4^{\circ}00' - 8^{\circ}00'N$ $155^{\circ}00'W$	22.06+	20.5	1.08	9
H.M. SMITH 33 (Mar.1955)	$4^{\circ}06' - 7^{\circ}23'N$ $140^{\circ}00'W$	10.40	9.7	1.07	9
H.M. SMITH 35 (Aug.1956)	$6^{\circ}09' - 9^{\circ}59'N$ $134^{\circ}45'W$	13.85	12.1	1.14	21

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P. E. C. C.)</u>	<u>Geostrophic Transport ($10^6 \text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4 \text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I. D. No.</u>
H.M. SMITH 35 (Oct.1956)	$3^{\circ}57' - 9^{\circ}59' \text{N}$ $160^{\circ}00' \text{W}$	41.02	22.4	1.83	22
H.M. SMITH 38 (Mar.1957)	$2^{\circ}01' \text{N} - 8^{\circ}56' \text{N}$ $145^{\circ}06' \text{W} - 149^{\circ}53' \text{W}$	15.46	14.2	1.09	62
H.M. SMITH 45 (April 1958)	$1^{\circ}00' - 3^{\circ}01' \text{N}$ $140^{\circ}00' \text{W}$	11.08+	14.4	.77	65
H.M. SMITH 45 (April 1958)	$1^{\circ}30' - 3^{\circ}26' \text{N}$ $140^{\circ}00' \text{W}$	0.75+	0.9	.82	66
STRANGER Equapac (Aug.1956)	$4^{\circ}02' - 9^{\circ}00' \text{N}$ $167^{\circ}00' \text{W}$	41.23	25.0	1.65	13
STRANGER Equapac (Sept.1956)	$4^{\circ}00' - 8^{\circ}09' \text{N}$ $175^{\circ}00' \text{W}$	35.80	21.5	1.67	12
STRANGER Doldrums (Aug.1958)	$5^{\circ}00' - 7^{\circ}00' \text{N}$ $107^{\circ}25' \text{W}$	24.63	7.8	3.16	67
STRANGER Doldrums (Aug.1958)	$4^{\circ}55' - 10^{\circ}00' \text{N}$ $107^{\circ}00' \text{W}$	20.94	11.7	1.79	68
TAKUYO (Jan.1958)	$1^{\circ}01' - 8^{\circ}26' \text{N}$ $153^{\circ}00' \text{E}$	67.23	20.4	3.30	29
TAKUYO (Feb.1958)	$2^{\circ}02' - 8^{\circ}30' \text{N}$ $151^{\circ}00' \text{E}$	36.64	19.4	1.89	30
TAKUYO (Feb.1958)	$1^{\circ}50' - 6^{\circ}04' \text{N}$ $149^{\circ}00' \text{E}$	39.15	16.3	2.40	31
UMITAKA-MARU (Nov.1958)	$2^{\circ}26' - 4^{\circ}59' \text{N}$ $135^{\circ}00' \text{E}$	42.53	17.8	2.39	35
VITYAZ 25 (July 1957)	$1^{\circ}31' - 4^{\circ}33' \text{N}$ $154^{\circ}00' \text{E}$	38.96	22.1	1.76	36

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P. E. C. C.)</u>	<u>Geostrophic Transport ($10^6 \text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4 \text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I. D. No.</u>
VITYAZ 25 (Aug. 1957)	$\frac{1^{\circ}54' \text{N} \quad 3^{\circ}57' \text{N}}{148^{\circ}22' \text{E} \quad 148^{\circ}01' \text{E}}$	32.15	23.4	1.37	37
VITYAZ 25 (Aug. 1957)	$\frac{2^{\circ}30' - 4^{\circ}00' \text{N}}{140^{\circ}00' \text{E}}$	32.01	14.1	2.27	38
VITYAZ 25 (Aug. 1957)	$\frac{0^{\circ}59' \text{N} \quad 4^{\circ}34' \text{N}}{134^{\circ}32' \text{E} \quad 134^{\circ}58' \text{E}}$	70.57	38.2	1.85	39
VITYAZ 25 (Aug. 1957)	$\frac{2^{\circ}38' \text{N} \quad 6^{\circ}10' \text{N}}{128^{\circ}27' \text{E} \quad 131^{\circ}50' \text{E}}$	39.12	17.3	2.61	40
VITYAZ 25 (Sept. 1957)	$\frac{2^{\circ}38' \text{N} \quad 5^{\circ}11' \text{N}}{128^{\circ}27' \text{E} \quad 126^{\circ}53' \text{E}}$	31.18	20.1	1.55	41
VITYAZ 26 (Nov. 1957)	$\frac{1^{\circ}08' \text{N} \quad 8^{\circ}34' \text{N}}{173^{\circ}00' \text{W} \quad 174^{\circ}07' \text{W}}$	37.93	24.8	1.53	42
VITYAZ 26 (Feb. 1958)	$\frac{2^{\circ}56' \text{N} \quad 9^{\circ}23' \text{N}}{172^{\circ}43' \text{E} \quad 173^{\circ}36' \text{E}}$	64.37	34.4	1.87	43
VITYAZ 27 (April 1958)	$\frac{2^{\circ}58' - 9^{\circ}38' \text{N}}{142^{\circ}00' \text{E}}$	48.50	25.3	1.92	44
VITYAZ 27 (April 1958)	$\frac{3^{\circ}32' - 7^{\circ}51' \text{N}}{143^{\circ}30' \text{E}}$	77.43	23.6	3.28	45
VITYAZ 27 (April 1958)	$\frac{5^{\circ}01' - 8^{\circ}00' \text{N}}{145^{\circ}00' \text{E}}$	17.84	15.5	1.15	46
VITYAZ 27 (April 1958)	$\frac{5^{\circ}27' \text{N} \quad 6^{\circ}14' \text{N}}{143^{\circ}33' \text{E} \quad 143^{\circ}28' \text{E}}$	12.07	3.1	3.89	47
VITYAZ 27 (April 1958)	$\frac{2^{\circ}58' - 5^{\circ}59' \text{N}}{145^{\circ}00' \text{E}}$	37.87	19.8	1.91	77
VITYAZ 27 (May 1958)	$\frac{2^{\circ}52' - 5^{\circ}02' \text{N}}{135^{\circ}30' \text{E}}$	32.07	16.5	1.94	78

TABLE I. (Continued)

TRANSPORT FUNCTIONS OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Hydrographic Cross-Section (P.E.C.C.)</u>	<u>Geostrophic Transport ($10^6\text{m}^3/\text{sec.}$)</u>	<u>Transport Function ($10^4\text{m}^2/\text{sec.}$)</u>	<u>Factor K (10^2)</u>	<u>I.D. No.</u>
VITYAZ 27 (May 1958)	$\frac{7^{\circ}00'N}{135^{\circ}20'E}$ $\frac{8^{\circ}40'N}{138^{\circ}06'E}$	5.99+	5.0	1.20	79

TABLE II.

THERMOCLINIC TRANSPORT OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Bathothermal Cross-Section (P.E.C.C.)</u>	<u>Thermoclinic Transport ($10^6 m^3/sec.$)</u>	<u>I. D. No.</u>
Acapulco Trench (Oct.1954)	$5^{\circ}45' - 10^{\circ}30'N$ $126^{\circ}00'W$	27.0	101
S.F. BAIRD Capricorn (Feb.1953)	$4^{\circ}15' - 8^{\circ}30'N$ $124^{\circ}00'W$	17.1	102
U.S.S. BARTON (July 1946)	$2^{\circ}00' - 6^{\circ}45'N$ $164^{\circ}30'E$	25.8	103
CAVALIERI (Aug.1952)	$4^{\circ}15' - 7^{\circ}00'N$ $140^{\circ}00'W$	7.2	104
CHALLENGER (Mar.1875)	$2^{\circ}15'N - 7^{\circ}45'N$ $146^{\circ}16'E - 144^{\circ}20'E$	34.2	105
CHALLENGER (Aug.1875)	$5^{\circ}54'N - 9^{\circ}28'N$ $147^{\circ}02'W - 150^{\circ}49'W$	16.2	106
GILBERT 1 (May 1952)	$5^{\circ}30' - 7^{\circ}30'N$ $120^{\circ}00'W$	6.2	107
GILBERT 1 (June 1952)	$5^{\circ}30' - 8^{\circ}45'N$ $130^{\circ}00'W$	19.7	108
GILBERT 15 (Mar.1954)	$5^{\circ}15' - 7^{\circ}15'N$ $110^{\circ}30'W$	2.2	109
GILBERT 15 (April 1954)	$4^{\circ}00' - 8^{\circ}30'N$ $155^{\circ}00'W$	18.9	110
Japanese (Feb.1935)	$5^{\circ}00' - 7^{\circ}00'N$ $136^{\circ}00'E$	16.3	111
Japanese (Jan.1936)	$4^{\circ}30' - 6^{\circ}30'N$ $138^{\circ}00'E$	44.7	112
Japanese (Feb.1936)	$4^{\circ}00' - 8^{\circ}00'N$ $149^{\circ}00'E$	50.0	113
U.S.S. LAFFEY (July 1946)	$4^{\circ}00' - 6^{\circ}45'N$ $167^{\circ}30'E$	27.9	114
MANNING 11 (Feb.1952)	$4^{\circ}30' - 8^{\circ}30'N$ $180^{\circ}00'$	28.8	115
MANNING 11 (Feb.1952)	$2^{\circ}30' - 6^{\circ}45'N$ $155^{\circ}00'W$	34.9	116
MANNING 11 (Mar.1952)	$3^{\circ}00' - 4^{\circ}15'N$ $169^{\circ}00'W$	4.7	117
MANNING 12 (Aug.1952)	$5^{\circ}00' - 8^{\circ}30'N$ $150^{\circ}00'W$	19.9	118
MANNING 13 (Oct.1952)	$6^{\circ}15'N - 10^{\circ}00'N$ $152^{\circ}30'W - 153^{\circ}30'W$	23.5	119
MANNING 13 (Nov.1952)	$3^{\circ}15' - 4^{\circ}30'N$ $168^{\circ}30'W$	4.8	120
MANNING 14 (Feb.1953)	$3^{\circ}45' - 8^{\circ}15'N$ $150^{\circ}00'W$	31.5	121
MANNING 14 (Mar.1953)	$2^{\circ}30' - 3^{\circ}00'N$ $140^{\circ}00'W$	2.8	122

TABLE II. (Continued)

THERMOCLINIC TRANSPORT OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Bathythermal Cross-Section (P.E.C.C.)</u>	<u>Thermoclinic Transport ($10^6 m^3/sec.$)</u>	<u>I. D. No.</u>
MANNING 15 (May 1953)	$7^{\circ}00' - 10^{\circ}00'N$ $150^{\circ}00'W$	0.8	123
MANNING 15 (June 1953)	$3^{\circ}30' - 7^{\circ}15'N$ $170^{\circ}00'W$	11.7	124
MANNING 16 (Aug.1953)	$3^{\circ}15' - 9^{\circ}30'N$ $155^{\circ}00'W$	20.2	125
MANNING 16 (Aug.1953)	$4^{\circ}30' - 9^{\circ}00'N$ $160^{\circ}00'W$	23.1	126
MANNING 18 (Dec.1953)	$4^{\circ}15' - 8^{\circ}30'N$ $155^{\circ}00'W$	44.0	127
SERRANO (May 1949)	$5^{\circ}15'N - 10^{\circ}30'N$ $125^{\circ}00'W - 123^{\circ}30'W$	5.1	128
SERRANO (May 1949)	$4^{\circ}15' - 8^{\circ}15'N$ $125^{\circ}30'W$	7.1	129
SHELLBACK (May 1952)	$6^{\circ}00'N - 8^{\circ}30'N$ $119^{\circ}00'W - 120^{\circ}30'W$	2.1	130
SHELLBACK (June 1952)	$4^{\circ}45' - 7^{\circ}30'N$ $97^{\circ}30' - 98^{\circ}00'W$	9.8	131
SHELLBACK (July 1952)	$2^{\circ}30' - 5^{\circ}00'N$ $85^{\circ}00'W$	5.5	132
SHELLBACK (Aug.1952)	$4^{\circ}15'N - 9^{\circ}00'N$ $89^{\circ}00'W - 88^{\circ}30'W$	3.8	133
SHELLBACK (Aug.1952)	$4^{\circ}30'N - 9^{\circ}00'N$ $102^{\circ}00'W - 104^{\circ}30'W$	9.4	134
H.M. SMITH 2 (Feb.1950)	$1^{\circ}30' - 10^{\circ}00'N$ $172^{\circ}00'W$	47.5	1
H.M. SMITH 2 (Feb.1950)	$5^{\circ}00' - 9^{\circ}30'N$ $158^{\circ}00'W$	25.5	2
H.M. SMITH 5 (July 1950)	$3^{\circ}45' - 7^{\circ}00'N$ $172^{\circ}00'W$	25.0	5
H.M. SMITH 5 (Aug.1950)	$5^{\circ}00' - 9^{\circ}30'N$ $158^{\circ}00'W$	28.9	3
H.M. SMITH 7 (Oct.1950)q	$5^{\circ}45'N - 10^{\circ}00'N$ $157^{\circ}00'W - 158^{\circ}00'W$	34.9	139
H.M. SMITH 7 (Nov.1950)	$5^{\circ}30'N - 9^{\circ}00'N$ $159^{\circ}00'W - 158^{\circ}15'W$	38.6	140
H.M. SMITH 8 (Jan.1951)	$4^{\circ}00' - 7^{\circ}30'N$ $158^{\circ}00'W$	40.5	4
H.M. SMITH 8 (Feb.1951)	$5^{\circ}00' - 6^{\circ}45'N$ $165^{\circ}30'W$	15.2	6
H.M. SMITH 8 (Mar.1951)	$4^{\circ}00' - 7^{\circ}30'N$ $172^{\circ}00'W$	37.4	7
H.M. SMITH 11 (Sept.1951)	$5^{\circ}30' - 8^{\circ}00'N$ $150^{\circ}00'W$	18.2	144

TABLE II. (Continued)

THERMOCLINIC TRANSPORT OF THE PACIFIC EQUATORIAL COUNTER-CURRENT

<u>Ship / Cruise</u>	<u>Bathythermal Cross-Section (P.E.C.C.)</u>	<u>Thermoclinic Transport ($10^6\text{m}^3/\text{sec.}$)</u>	<u>I. D. No.</u>
H.M. SMITH 11 (Sept.1951)	$3^{\circ}30' - 8^{\circ}30'N$ $150^{\circ}00'W$	34.3	8
H.M. SMITH 14 (Jan.1952)	$5^{\circ}30' - 9^{\circ}30'N$ $155^{\circ}00'W$	25.5	9
H.M. SMITH 14 (Feb.1952)	$4^{\circ}00' - 8^{\circ}30'N$ $180^{\circ}00'$	28.3	147
H.M. SMITH 14 (Mar.1952)	$3^{\circ}15' - 6^{\circ}00'N$ $169^{\circ}00'W$	22.3	148
H.M. SMITH 15 (May 1952)	$4^{\circ}30' - 8^{\circ}30'N$ $140^{\circ}00'W$	16.4	149
H.M. SMITH 15 (June 1952)	$5^{\circ}00' - 8^{\circ}00'N$ $140^{\circ}00'W$	14.6	150
H.M. SMITH 15 (June 1952)	$5^{\circ}00' - 8^{\circ}00'N$ $140^{\circ}00'W$	16.0	151
H.M. SMITH 15 (June 1952)	$4^{\circ}45' - 8^{\circ}45'N$ $140^{\circ}00'W$	18.7	152
H.M. SMITH 16 (July 1952)	$5^{\circ}00' - 8^{\circ}45'N$ $150^{\circ}00'W$	22.1	153
H.M. SMITH 18 (Oct.1952)	$5^{\circ}15'N - 9^{\circ}15'N$ $120^{\circ}00'W - 121^{\circ}00'W$	27.9	154
H.M. SMITH 18 (Nov.1952)	$5^{\circ}45' - 8^{\circ}45'N$ $131^{\circ}00'W$	40.7	155
H.M. SMITH Equapac (Oct.1955)	$5^{\circ}30' - 10^{\circ}45'N$ $110^{\circ}00'W$	9.5	156
H.M. SMITH Equapac (Oct.1955)	$3^{\circ}00' - 5^{\circ}30'N$ $140^{\circ}00'W$	9.6	157
TENYO-MARU (Aug.1951)	$1^{\circ}00' - 7^{\circ}00'N$ $150^{\circ}00'E$	27.4	158
TENYO-MARU (Sept.1951)	$2^{\circ}00' - 9^{\circ}30'N$ $160^{\circ}00'E$	25.7	159

TABLE III.

TABULATED TRANSPORTS BY MONTH AND LONGITUDE

	LONGITUDE																
	120°E	140°E	160°E	180°	160°W	140°W	120°W	100°W	80°W								
JANUARY	23 11	45	67		29 22												
FEBRUARY	16	16	50 39	37	64	29 28	25	17	20 35	32	17	18					
MARCH		34			20	22 5	15	10 3			2						
APRIL		49	12 77	18 38	69				19	11 1							
MAY	32	6			4		1	16	7 5	2 6							
JUNE					12			19 15 16	20 16		10						
JULY		86	39	26	28	44	26	22	21		6	8	6				
AUGUST	68 39	71	32 40	59 21	27 37	47	46		41	23 22	20 16	24	7	14	25 21	10	4
SEPTEMBER	31		26		36		26	18									
OCTOBER								41	24		10	40	27	12	13	7	10
NOVEMBER		43				38	5	39	23		41				1 6	3 5	5
DECEMBER					62		44						20	15	13		

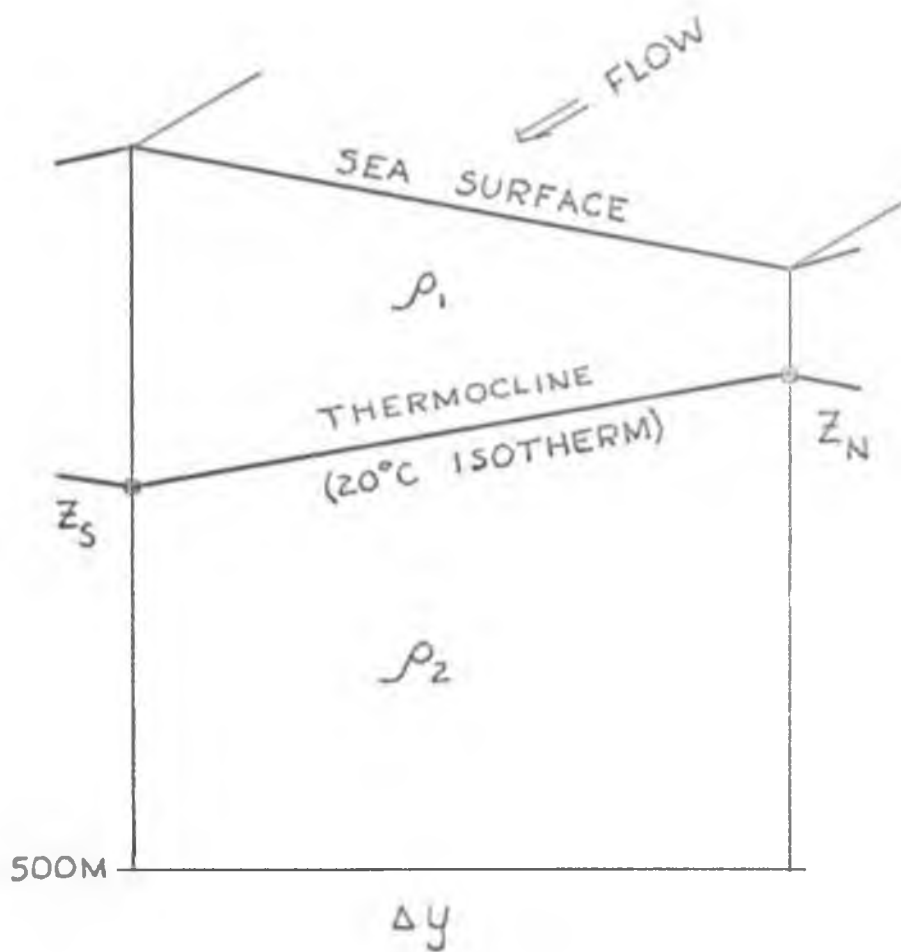


FIGURE 1. MERIDIONAL SECTION OF THE PACIFIC EQUATORIAL COUNTERCURRENT

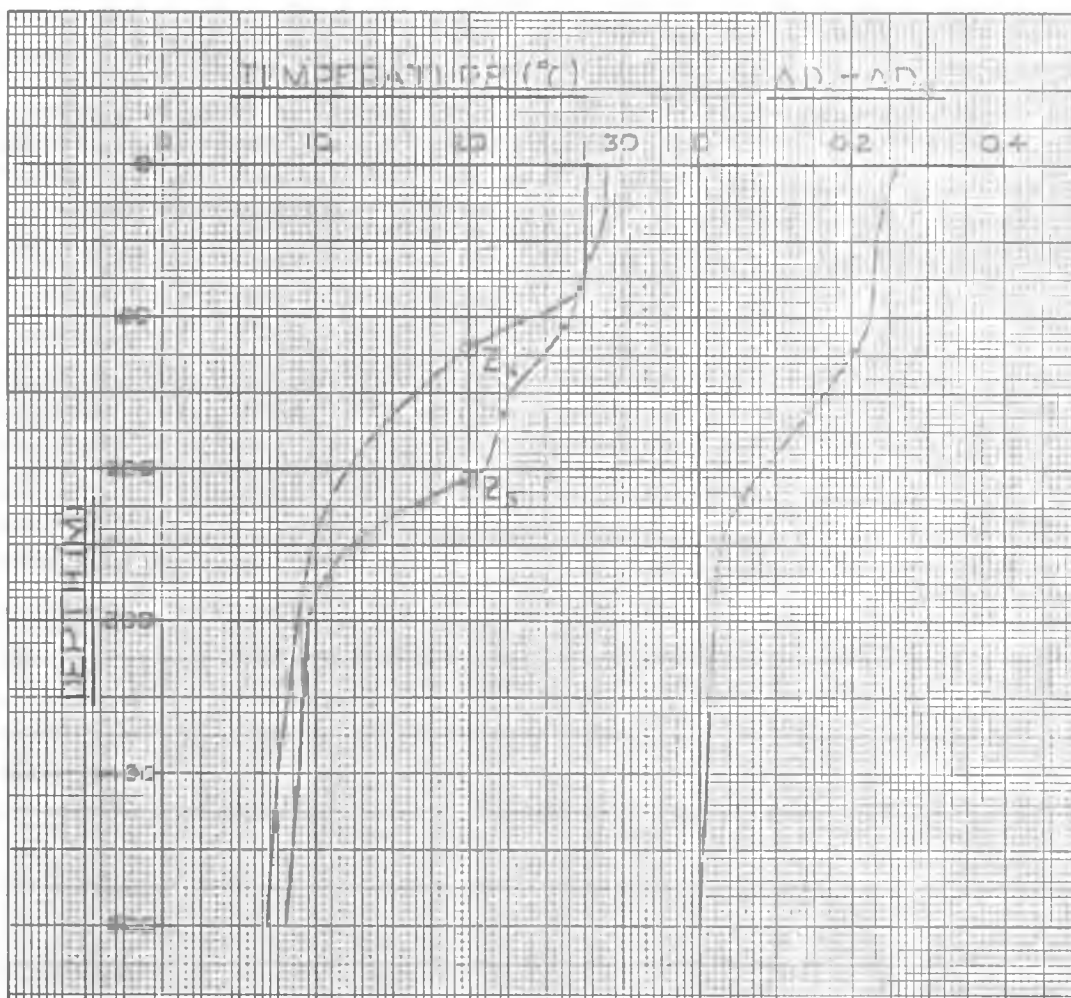


FIGURE 2. VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A VITYAZ SECTION AT 142°E (IDENTIFICATION NO. 44)

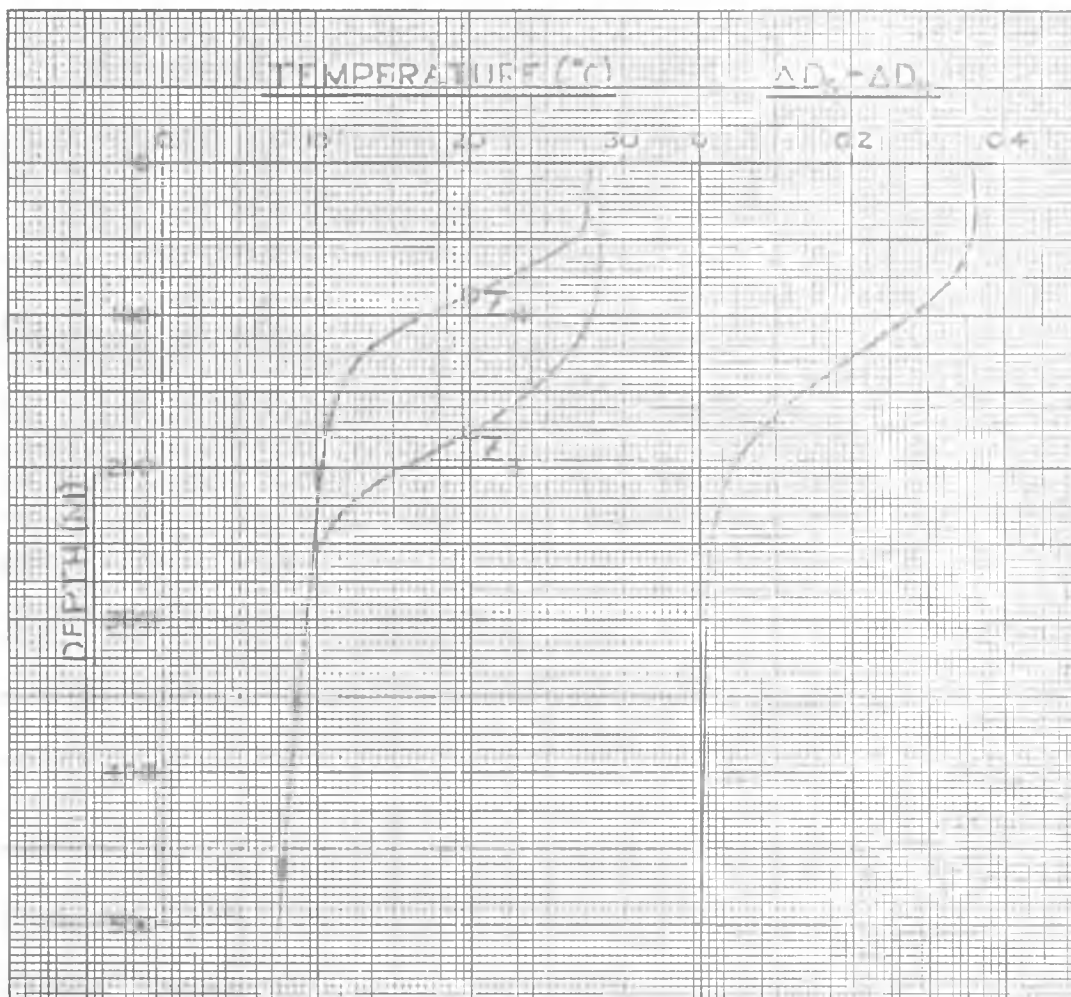


FIGURE 3. VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A STRANGER SECTION AT 175°W (IDENTIFICATION NO. 12)

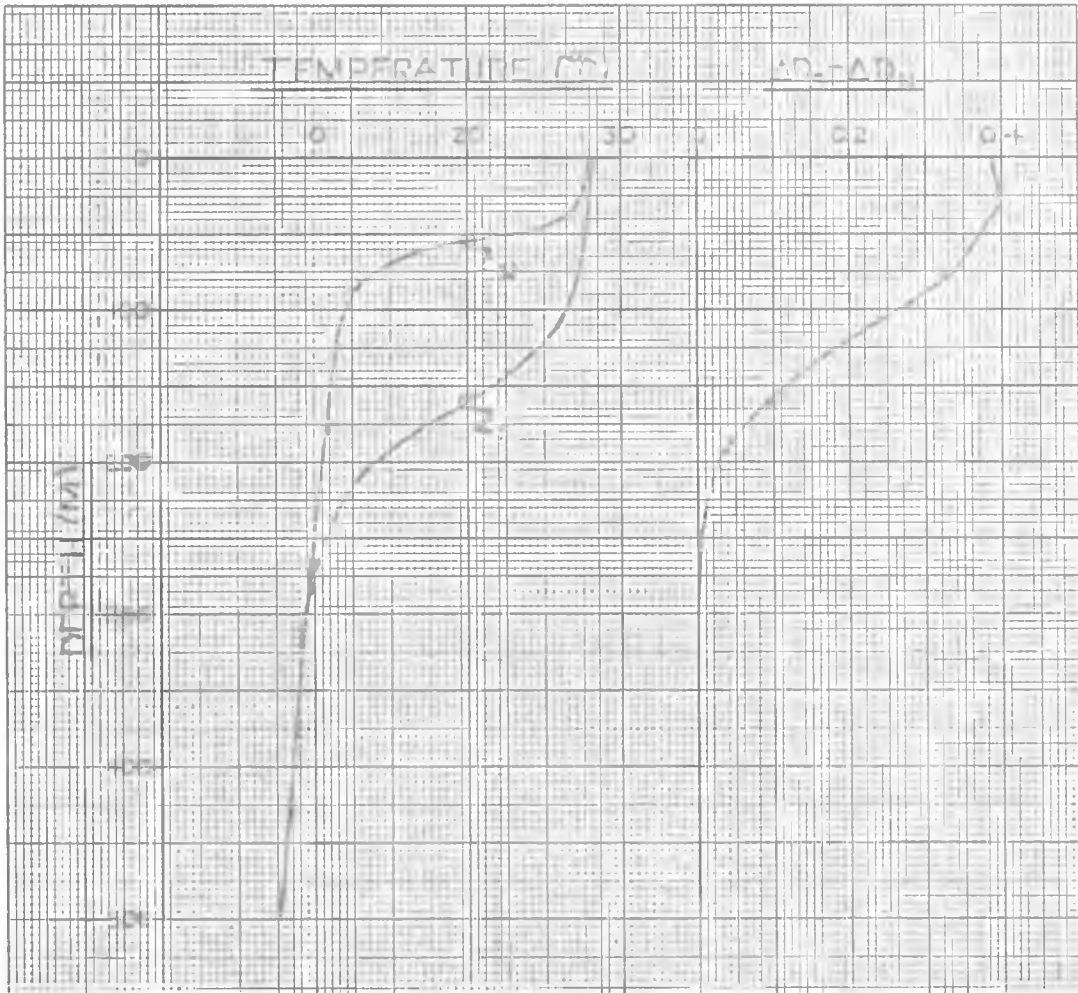


FIGURE 4. VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A HUGH M. SMITH SECTION AT 150°W (IDENTIFICATION NO. 8)

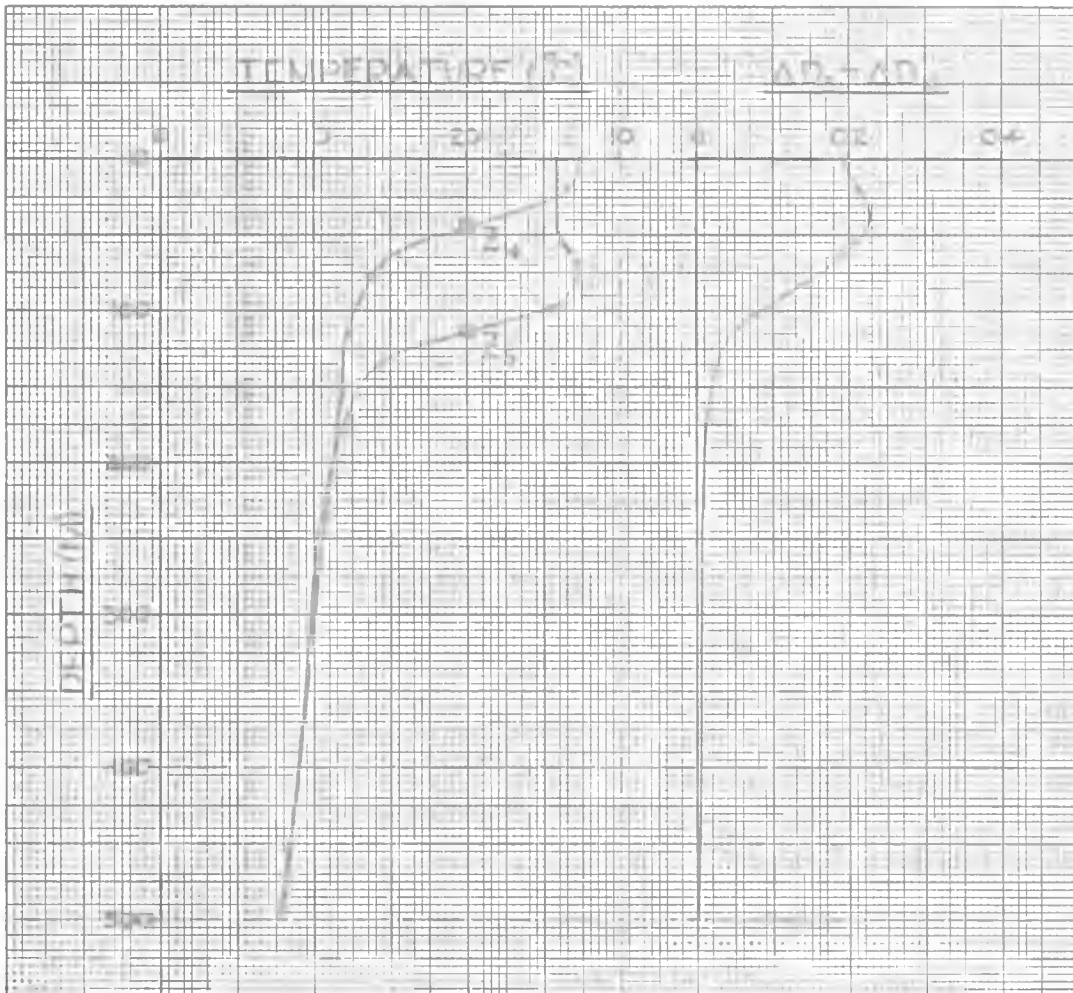


FIGURE 5. VERTICAL DISTRIBUTION OF TEMPERATURE AT THE NORTHERN AND SOUTHERN BOUNDARY OF THE COUNTERCURRENT AND OF THE DIFFERENCE OF DYNAMIC HEIGHT BETWEEN THESE TWO LOCATIONS FROM THE SURFACE TO 500 METER DEPTH ALONG A S. F. BAIRD SECTION AT 115°W (IDENTIFICATION NO. 49)

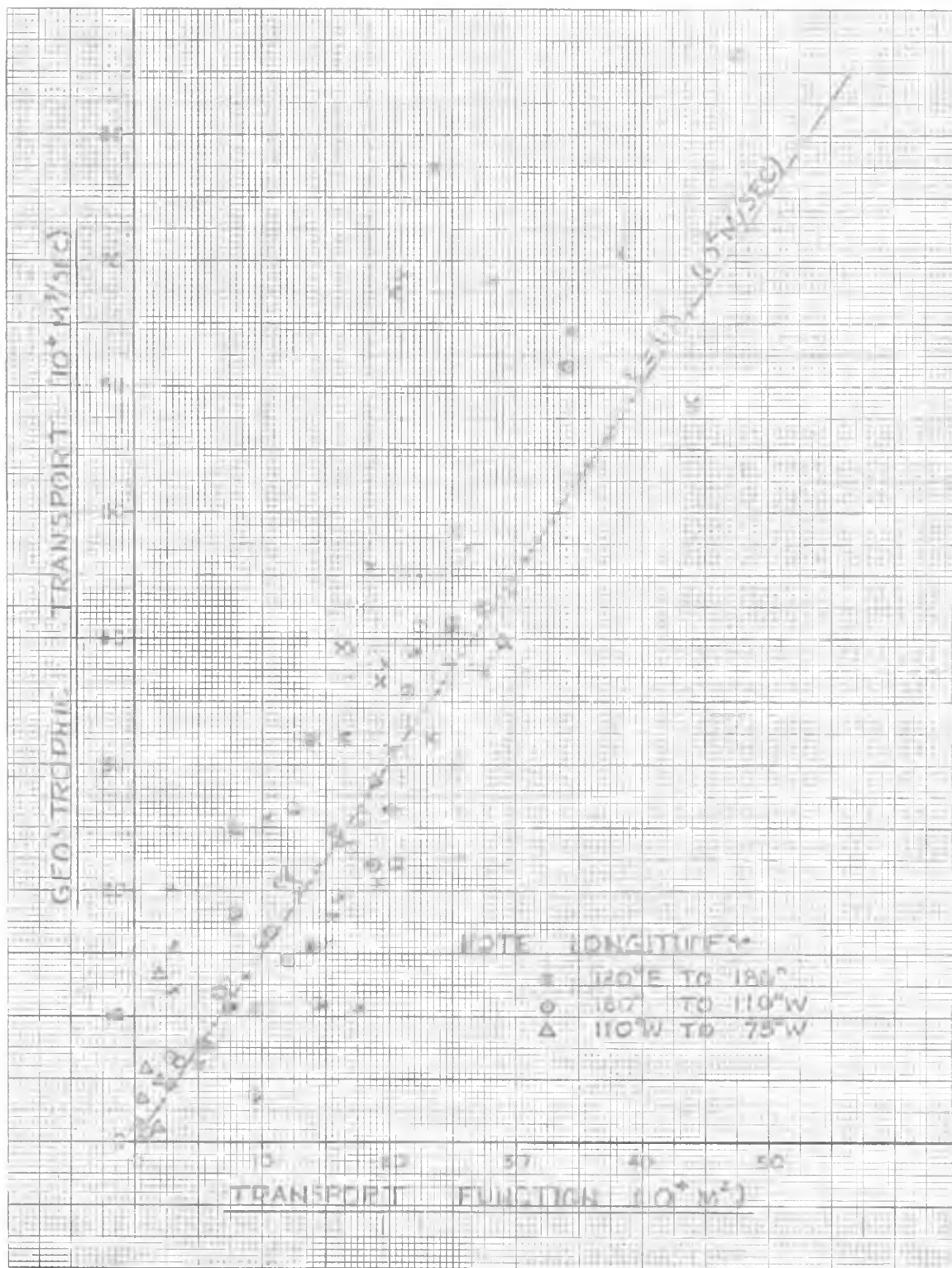
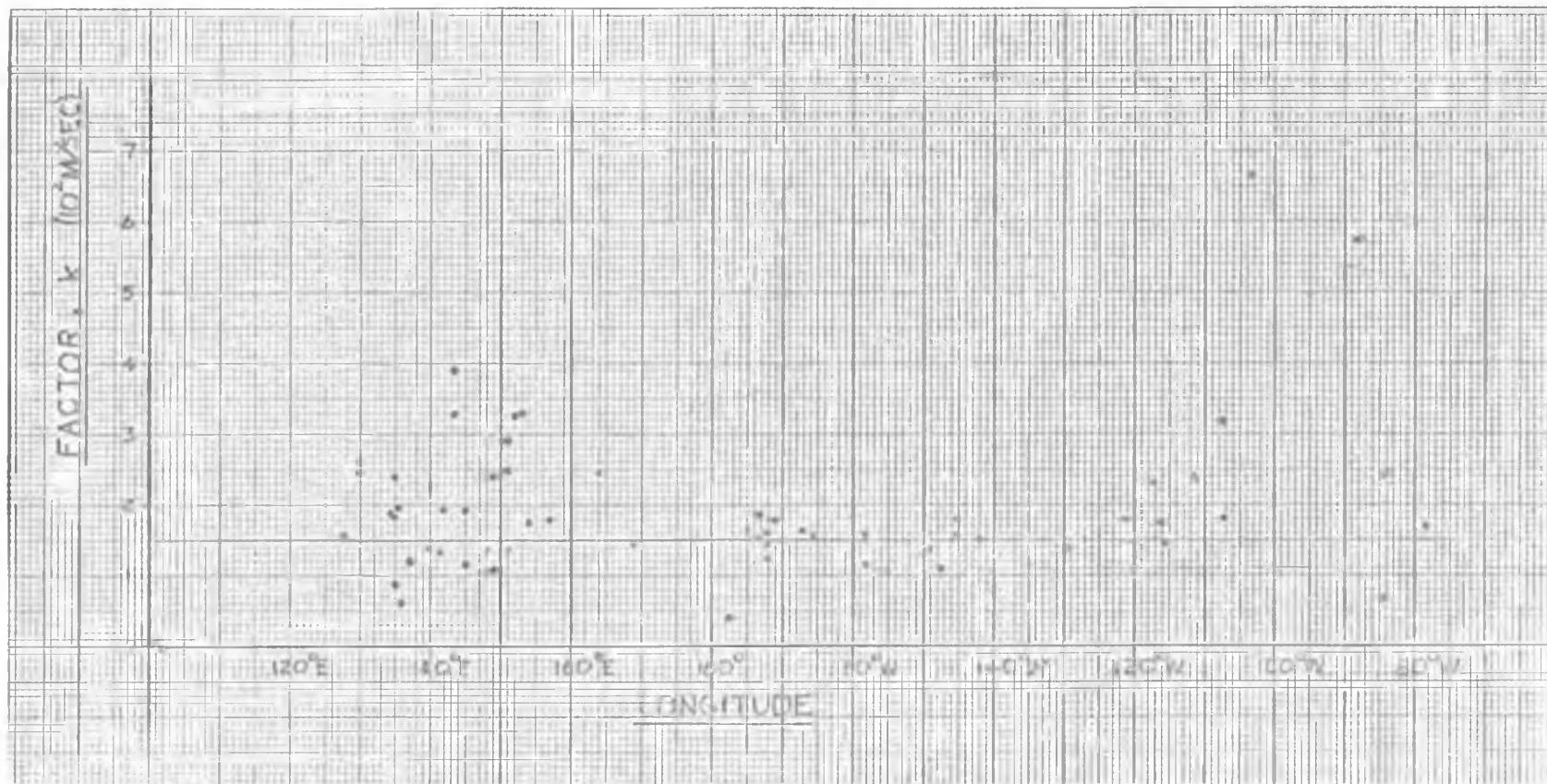


FIGURE 6. GEOSTROPHIC TRANSPORT VERSUS TRANSPORT FUNCTION WITH LONGITUDE REGIONS AND A FACTOR $K = 1.5$ NOTED



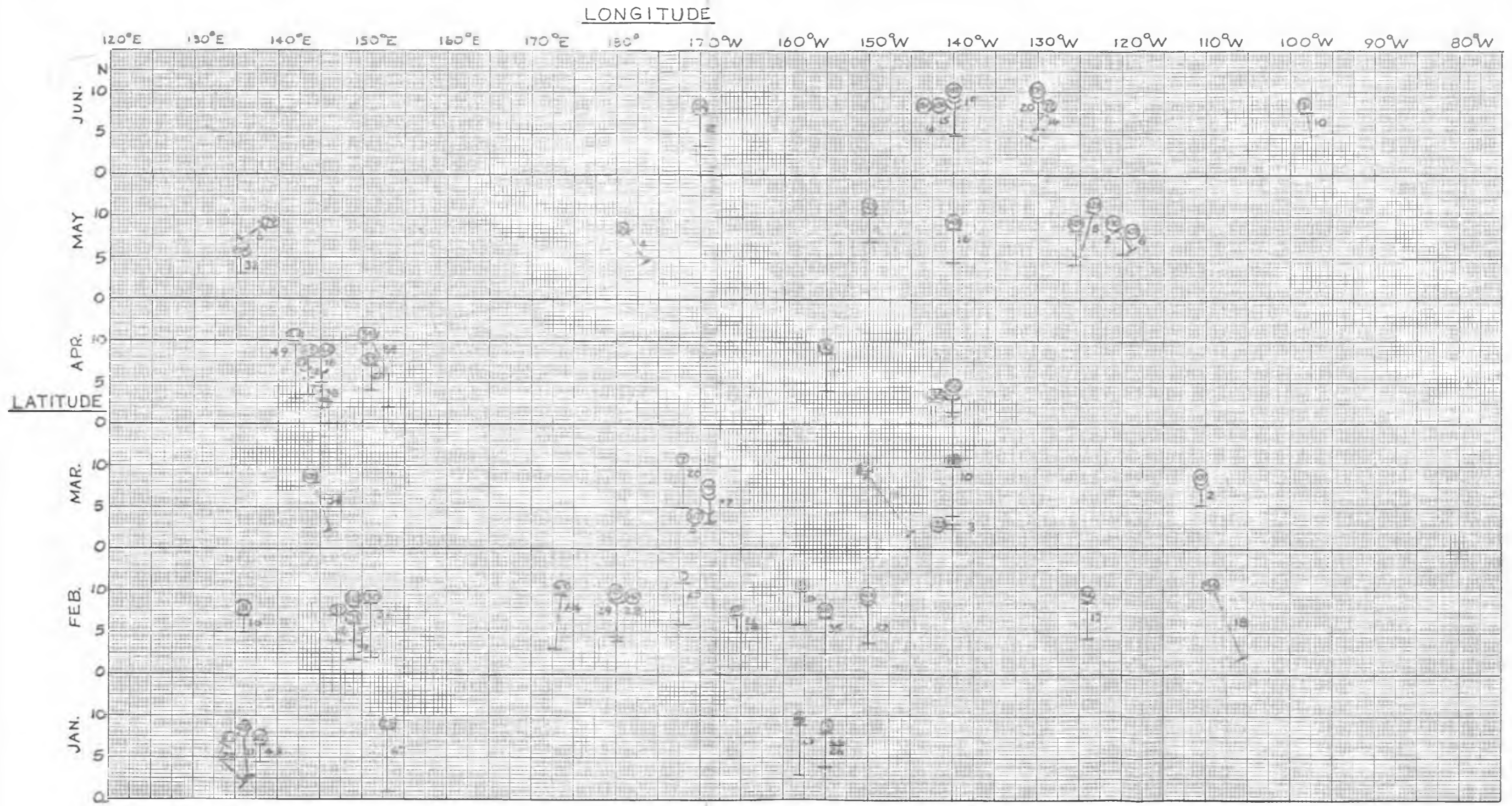


FIGURE 8. POSITIONS OF COUNTERCURRENT SECTIONS INDICATING RANGE AND TRANSPORT MAGNITUDES ($10^6 \text{M}^3/\text{SEC.}$) FOR THE MONTHS OF JANUARY THROUGH JUNE. CIRCLED IDENTIFICATION NUMBERS REFER TO TABLES I AND II

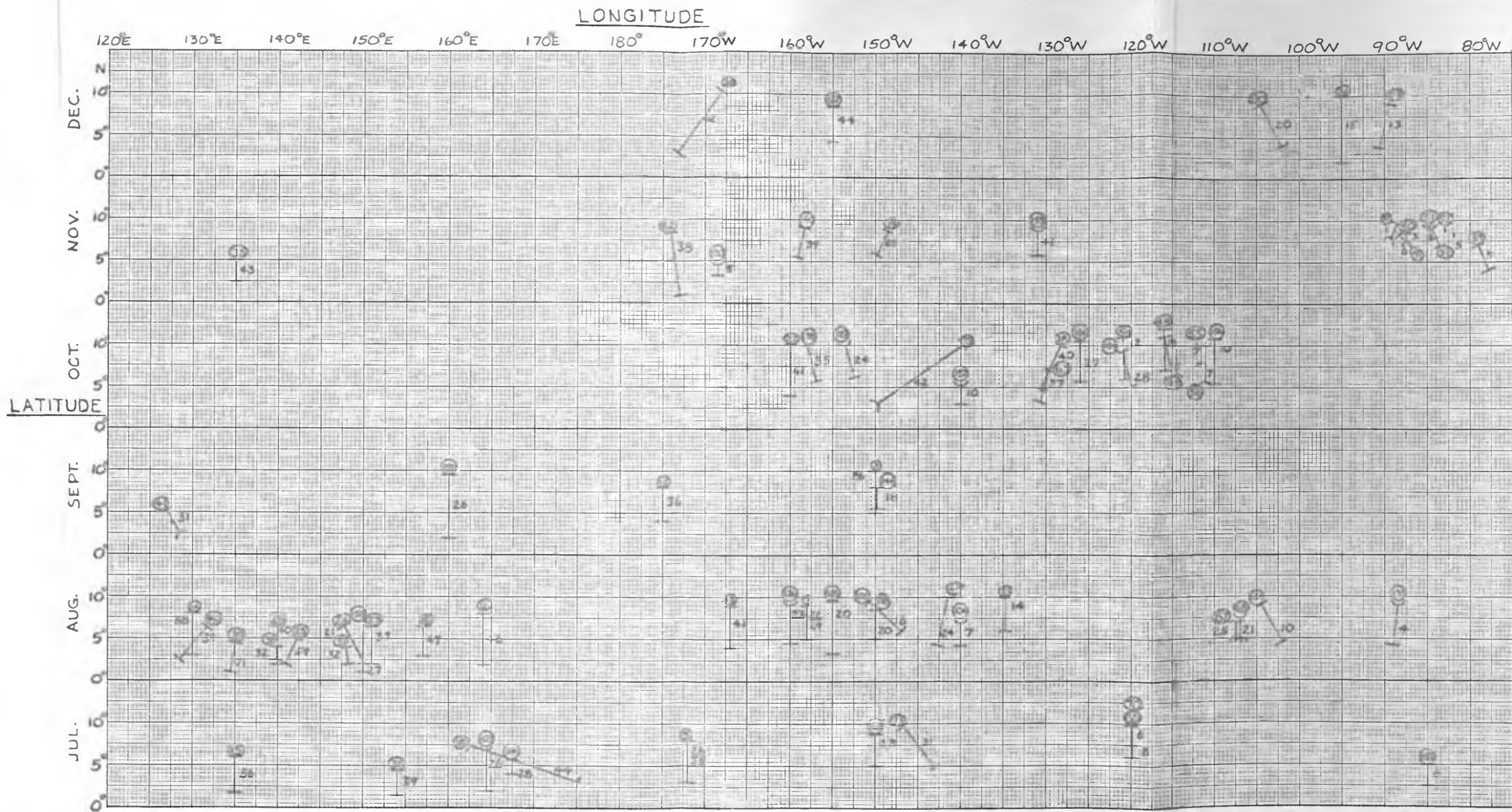


FIGURE 9. POSITIONS OF COUNTERCURRENT SECTIONS INDICATING RANGE AND TRANSPORT MAGNITUDES ($10^6 \text{M}^3/\text{SEC.}$) FOR THE MONTHS OF JULY THROUGH DECEMBER
CIRCLED IDENTIFICATION NUMBERS REFER TO TABLES I AND II

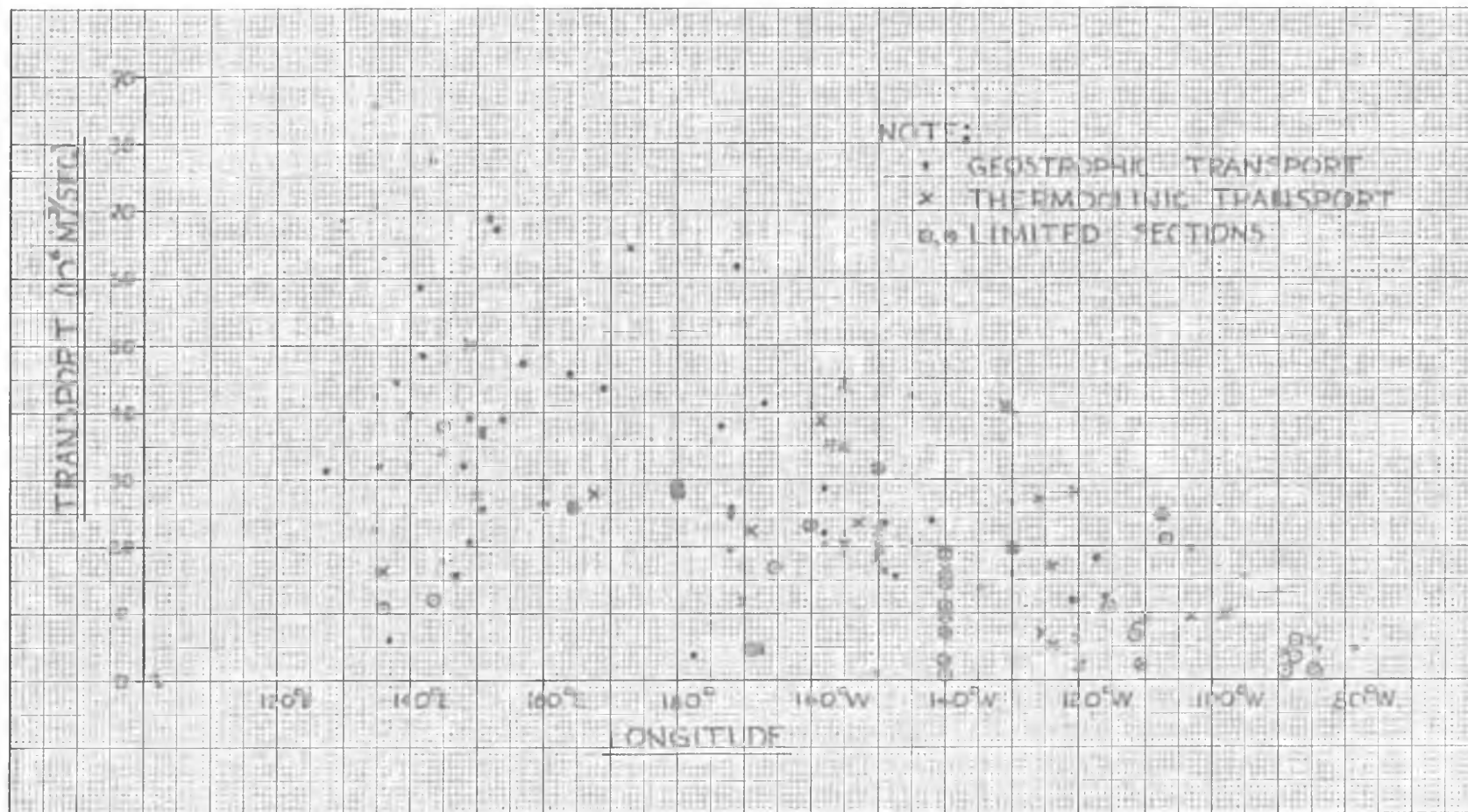


FIGURE 10. GEOSTROPHIC AND THERMOCLINIC TRANSPORTS VERSUS LONGITUDE WITH LIMITED SECTIONS NOTED

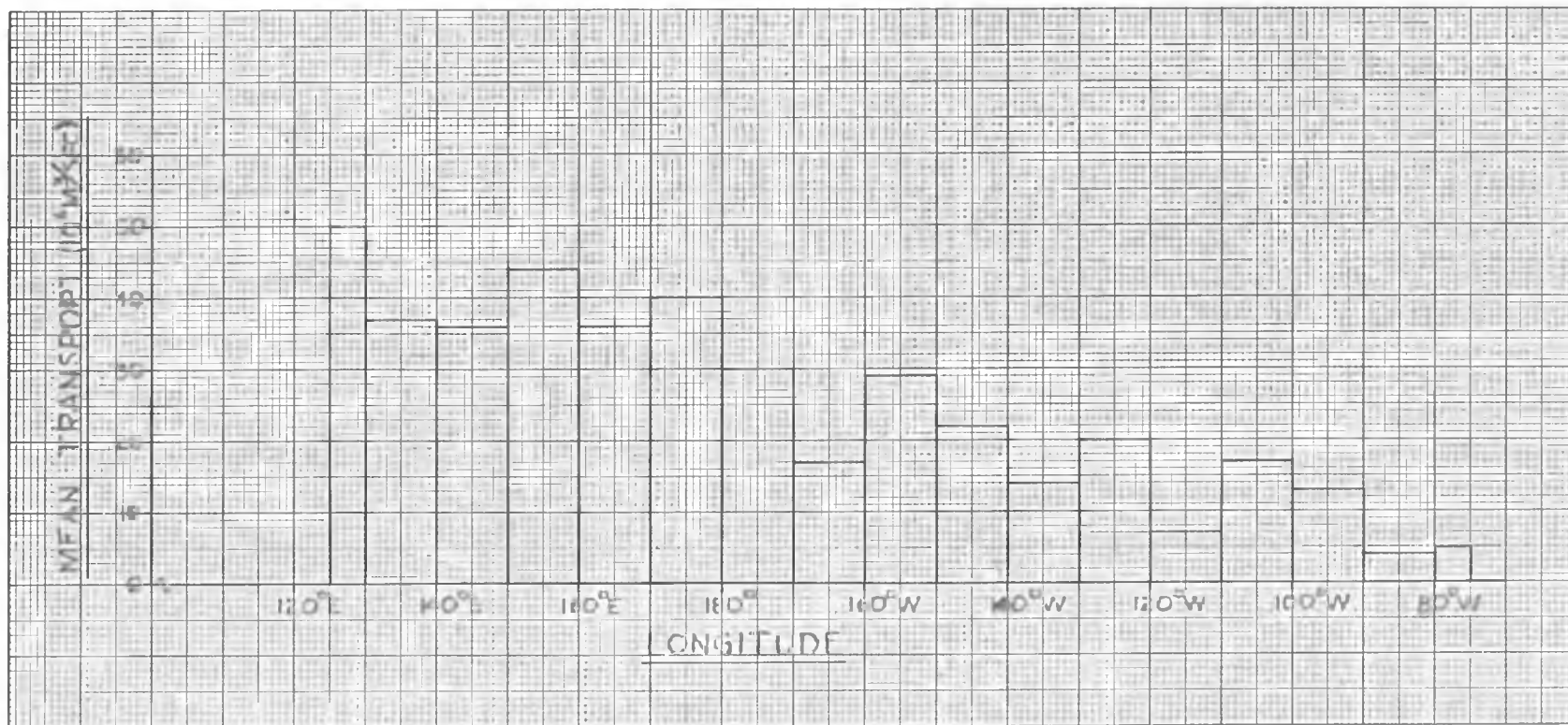


FIGURE 11. MEAN TRANSPORTS FOR INCREMENTS OF LONGITUDE

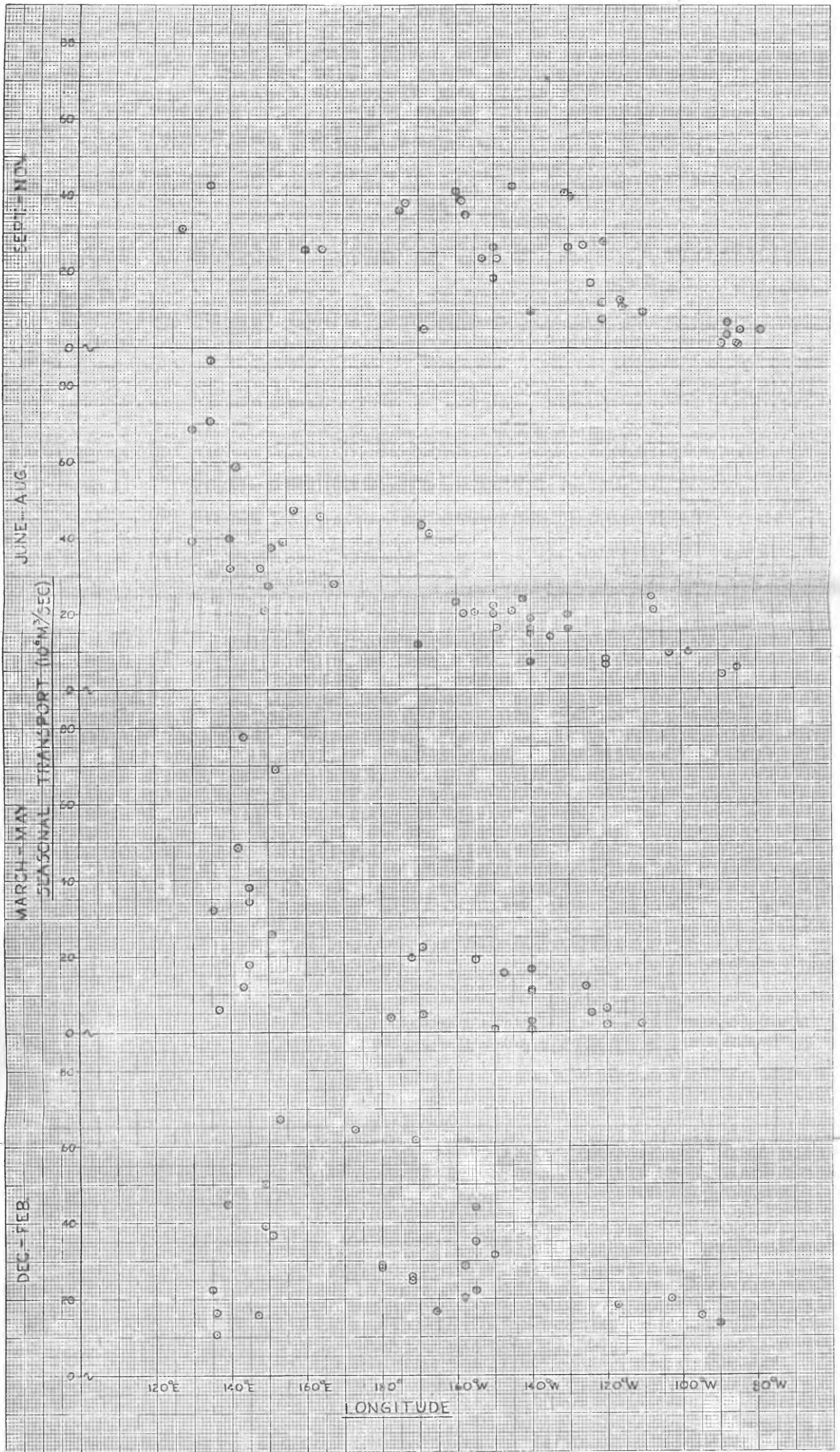


FIGURE 12. SEASONAL TRANSPORTS VERSUS LONGITUDE